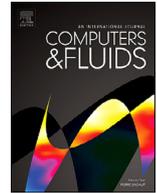




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# Turbulence in realistic geometries with moving boundaries: When simulations meet experiments

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## ABSTRACT

Considering the current advances in experimental capabilities in fluid mechanics and the advances in computing power and numerical methods in computational fluid mechanics, a question that naturally arises is whether the two sets of techniques are approaching a level of sophistication sufficiently high to deliver results on turbulent flows in realistic geometries that are comparable. The purpose of this paper is to give elements of answers to this question by considering the so-called von Kármán flow where the fluid in a cylindrical container is driven by two counter-rotating impellers. We compare in the mentioned flow the torque and the flow topology obtained by experiments, direct numerical simulations (DNS), and large eddy simulations (LES) at various Reynolds numbers ranging from  $Re = \mathcal{O}(10^2)$  to  $Re = \mathcal{O}(10^5)$ . In addition to validating the proposed LES model, the level of agreement that is observed between the numerical and the experimental data shows that the degree of accuracy of each of these techniques is reaching a threshold beyond which it is possible to use each of them with high confidence to explore and better understand turbulence in complex flows at  $Re = \mathcal{O}(10^5)$  and beyond.

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## 1. Introduction

The equations modeling the motion of incompressible homogeneous fluids are well-established. Denoting by  $\mathbf{u}$  the three-dimensional velocity field,  $p$  the pressure,  $\rho$  the (constant) density,  $\mathbf{f}$  the forcing, and  $\nu$  the kinematic viscosity, the incompressible Navier-Stokes equations take the following form:

$$\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} = -\frac{1}{\rho} \nabla p + \nu \Delta \mathbf{u} + \mathbf{f}, \quad (1)$$

$$\nabla \cdot \mathbf{u} = 0. \quad (2)$$

It is known since the pioneering work of Reynolds that after proper rescaling of the equations by  $L$  and  $U$ , some characteristic length

and velocity scales, the Navier-Stokes equations only depend on one parameter: the Reynolds number  $Re := LU/\nu$ . The above system of balance equations is simple to formulate, but this apparent simplicity is deceiving since the Navier-Stokes system is the source of the notoriously hard problem commonly referred to as turbulence [1].

Over the years, two competing strategies have been used to advance the understanding of turbulence: numerical simulations and laboratory experiments. The constant progresses made in computer technology, computing techniques, and imaging softwares have pushed the limits of applicability of both numerical simulations and laboratory experiments. For instance, the availability of larger parallel computers and progresses made in parallel linear algebra libraries now allow Direct Numerical Simulation (DNS) and turbulence models, like Large Eddy Simulation (LES), to handle larger Reynolds numbers and to perform longer time statistics. Recent algorithmic progresses made on penalty methods now allow to use Fourier techniques to simulate complex geometries,

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thereby unlocking the power of highly performant spectral methods. Similarly, technological progresses over the years have steadily increased experimental capabilities. For instance, the use of CCD cameras combined with the continuous increase of the performance of computers have made digital particle image velocimetry a very accurate tool, which is now widely available. Particle image velocimetry (PIV) gives access to all the velocity components in laboratory experiments.

A natural question that comes to mind is whether we are at a point where numerical techniques and laboratory experiments have reached a common ground where both techniques can be used at the same time to investigate the same complex flow, at the same values of the control parameter, and be either compared to each other or used to complement each other in order to advance the theory of turbulence. One goal of this paper is to give elements of answer to this question. The other two goals of the paper are to validate the performance of two numerical techniques: (i) an entropy viscosity LES technique and (ii) a pseudo-penalty technique to simulate moving boundaries. Comparisons between LES (and/or DNS) simulations and experimental results have already been conducted on similar setups [2–4], but the experimental data used therein were obtained from the literature. Instead here we produce both experimental and numerical results in the very same configuration.

In the present paper we focus our attention on the so-called von Kármán flow which consists of a fluid in a cylindrical container driven by a pair of counter-rotating impellers. The turbulence generated in this setup is neither isotropic, nor homogeneous, and is therefore an example of turbulence in a complex geometry that is rarely discussed in the turbulence literature. To account for the moving impellers driving the fluid in the numerical simulations, we adapt the pseudo-penalty method by [5] to a mixed finite element/Fourier approximation setting. We also adopt an entropy-viscosity-based LES technique to handle large Reynolds numbers. We demonstrate in this paper that in this setting the combination of the pseudo-penalty method and the entropy-viscosity-based LES model allows us to reach levels of accuracy that are comparable to laboratory experiments. By carefully comparing global and local indicators of turbulence at similar values of  $Re$ , we show that the numerical simulations and the laboratory experiments agree with each other for Reynolds numbers ranging from  $Re = \mathcal{O}(10^2)$  up to  $Re = \mathcal{O}(10^5)$ . Moreover, the numerical simulations reproduce different bifurcated states of the turbulent flows (i.e., turbulent states that break symmetries and coexist at the same high Reynolds number) that are experimentally observed.

The paper is organized as follows. In Section 2 we describe the von Kármán flow together with the relevant control parameters. The numerical methods used to approximate the Navier-Stokes equations with moving solid obstacles are described in Section 3. We also briefly describe in this section the entropy viscosity stabilization model that allows us to approximate large Reynolds number flows with coarse meshes. Section 4 introduces the experimental setup and additional parameters that characterize von Kármán flows. Comparisons between the experimental results and the numerical simulations are done in Section 5. One highlight of this section is Fig. 15 where we compare experimental measurements of the global energy dissipation in the considered setup with numerical simulations in the range  $Re \in [10, 10^5]$ . Concluding remarks are reported in Section 7.

## 2. Setup description

The von Kármán (VK) flow is produced by the stirring of a fluid contained in a cylindrical tank. This setup has been extensively studied using various fluids such as glycerol, water, air, helium gas, superfluid helium, etc. [6–11], since it is a canonical configuration

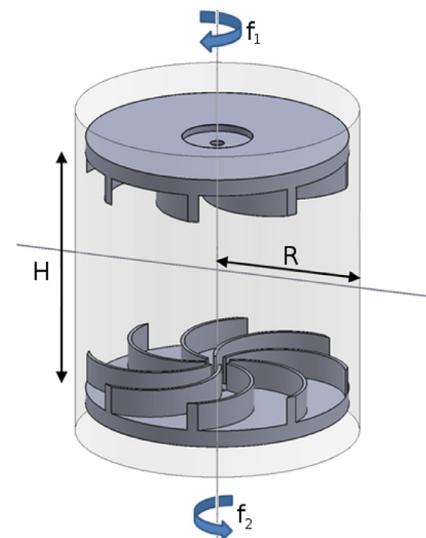


Fig. 1. Experimental setup with  $H$  the distance between the inner faces of the disks,  $R$  the cylinder radius,  $f_i$  the frequency of each disk. Impellers with 8 blades are called TM87. The arrows show the rotation direction for the CONTRA configuration.

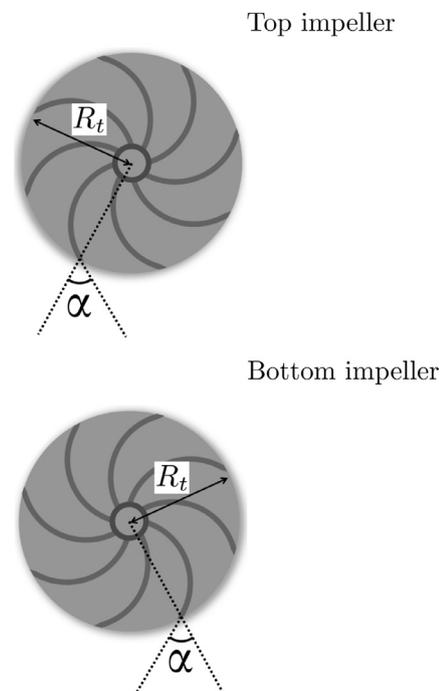


Fig. 2. TM87 impellers (8 blades) with radius  $R_t$  and angle  $|\alpha| = 72^\circ$ . The supporting disks are in the background, the blades are in the foreground, the shafts are behind the supporting disks.

for the investigation of turbulence in a confined geometry. The radius and height of the cylindrical vessel are denoted  $R$  and  $H_v$ , respectively. The stirring is done with two counter-rotating impellers that are separated by a distance denoted  $H$ . A schematic representation of the experimental setup is shown in Fig. 1 and a sketch of the impellers is shown in Fig. 2. The impellers may rotate at different signed frequencies  $f_1$  and  $f_2$ . In the present paper, we focus our attention on the cases where the two impellers are counter-rotating at the same frequency, i.e.,  $f_i := |f_1| = |f_2|$  and  $f_1 = -f_2$ . Looking at Fig. 1, we adopt the following conventions: the vertical axis is oriented upward, and we use the right-hand rule to define the sign of rotations about the vertical axis. For instance, for the situation shown in Fig. 1 the bottom impeller rotates in

the positive direction and the top impeller rotates in the negative direction; that is  $0 \leq f_2 = -f_1$ . This operating condition is referred to in the rest of the paper with the adjective CONTRA. Similarly when  $-f_1 = f_2 \leq 0$ , we say that the configuration is ANTI. Notice that the CONTRA and the ANTI operating conditions produce different flows since the blades are curved as shown in Fig. 2. The convention adopted in Fig. 2 is that the supporting disk is in the background, the blades are in the foreground, and the shaft is behind the supporting disk. In this figure, the bottom impeller works in the CONTRA condition when it rotates counter-clockwise, and it works in the ANTI condition when it rotates clockwise. The ANTI flow regime is characterized by a larger level of fluctuations and larger energy dissipation than the CONTRA regime; as will be shown below, it is also subject to a spontaneous symmetry breaking bifurcation of the mean flow topology.

In the entire paper, all the velocity fields are non-dimensionalized using the typical forcing velocity  $V_0 := 2\pi R f_i$  based on the radius of the cylinder and the rotation frequency of the impellers. The control parameter of the VK flow is the *Reynolds number*, defined as:

$$Re := 2\pi f_i R^2 \nu^{-1}. \quad (3)$$

Unless explicitly specified otherwise, all the lengths are now expressed in units of the cylinder radius  $R$ .

### 3. Numerical approximation method

The simulations corresponding to the VK experimental setup have been done using a code henceforth referred to as SFEMaNS (for Spectral/Finite Elements code for Maxwell and Navier-Stokes equations). This section describes the algorithm we have adopted to represent the moving solid obstacles like the counter-rotating impellers shown on Fig. 2. The convergence of the method is demonstrated with analytical tests. We also describe the LES model we use to compute large Reynolds number flows on grids that are not fine enough to represent the viscous dissipation scales.

#### 3.1. Frame of work: The code SFEMaNS

SFEMaNS uses a hybrid spatial discretization combining spectral and finite elements. In a nutshell the approximation in space is done by using a Fourier decomposition in the azimuthal direction and the continuous Hood-Taylor Lagrange element  $\mathbb{P}_1 - \mathbb{P}_2$  (linear approximation for pressure and quadratic approximation for the velocity in the meridian section). All the discrete functions  $A$  are written in the generic form:

$$A(r, \theta, z, t) = A_h^{0,\cos}(r, z, t) + \sum_{m=1}^M A_h^{m,\cos}(r, z, t) \cos(m\theta) + \sum_{m=1}^M A_h^{m,\sin}(r, z, t) \sin(m\theta), \quad (4)$$

with  $(r, \theta, z)$  the cylindrical coordinates,  $t$  the time and  $M$  the number of Fourier modes considered. The functions  $A_h^{m,\cos}$  and  $A_h^{m,\sin}$  belong to a finite element space (piecewise linear approximation for pressure and piecewise quadratic approximation for the velocity). The approximation in time is done by using a pressure-correction method described in [12]. The moving counter-rotating impellers are accounted for by using a pseudo-penalty technique described in [5]. The full algorithm is detailed in Section 3.2. Modulo the computations of nonlinear terms with the fast Fourier transform, the linear problems at each time step for each Fourier mode in the meridian section are uncoupled and are thereby parallelized by using the message passing interface. The solution

of each linear problem in the meridian section is further parallelized by using graph partitioning techniques from the METIS library [13] and subroutines from the portable extensible toolkit for scientific computation library (PETSc) [14], for the linear algebra. SFEMaNS has been thoroughly validated on numerous manufactured solutions and against other hydrodynamic codes [15–18].

#### 3.2. Algorithm to enforce moving domains

Since the impellers move with opposite angular velocities, it is impossible to find a frame of reference where the fluid domain is time-independent. This problem is addressed by combining into a single computational domain the counter-rotating impellers,  $\Omega_{\text{solid}}(t)$ , and the fluid domain,  $\Omega_{\text{fluid}}(t)$ . Using the cylindrical coordinate system  $(r, \theta, z)$  about the vertical axis with the convention that the vertical axis is oriented upwards, we then define the indicator function of the fluid domain,  $\chi$ , as follows:

$$\chi(r, \theta, z, t) = \begin{cases} 1 & \text{if } (r, \theta, z) \in \Omega_{\text{fluid}}(t) \\ 0 & \text{if } (r, \theta, z) \in \Omega_{\text{solid}}(t). \end{cases} \quad (5)$$

As shown in [19], the problem can be reformulated in the global computational domain by adding a penalty term of the form  $(1 - \chi)(\mathbf{u} - \mathbf{u}_{\text{obst}})/\alpha$  on the left-hand side of the momentum Eq. (1) where  $\alpha$  is a user-dependent penalty parameter and  $\mathbf{u}_{\text{obst}}$  the velocity of the disks and the blades given by:

$$\mathbf{u}_{\text{obst}}(r, \theta, z) = \begin{cases} -\text{sgn}(f_2) r \mathbf{e}_\theta & \text{if } z > 0, \\ \text{sgn}(f_2) r \mathbf{e}_\theta & \text{if } z \leq 0, \end{cases} \quad (6)$$

with  $\text{sgn}(f_2)$  equal to 1 if  $f_2 > 0$ , 0 if  $f_2 = 0$ , and  $-1$  otherwise. A significant difficulty with this formulation when working with the Fourier approximation is that the term  $\chi \mathbf{u}$  involves FFTs and thereby cannot be made implicit. An elegant solution to this problem has been proposed in [5]. It is showed therein that the problem can also be reformulated by solving the following balance equations:

$$(1 - \chi) \frac{\mathbf{u} - \mathbf{u}_{\text{obst}}}{\alpha} - \frac{1}{Re} \Delta \mathbf{u} + \nabla p = \chi (-\partial_t \mathbf{u} - (\nabla \times \mathbf{u}) \times \mathbf{u} + \mathbf{f}), \quad (7a)$$

$$\nabla \cdot \mathbf{u} = 0, \quad (7b)$$

where  $\mathbf{u}$  is the velocity field,  $p$  is the pressure field,  $\mathbf{f}$  is the forcing term introduced in Eq. (1) and  $\alpha$  is a penalty parameter. The key idea in [5] is the observation that replacing  $\alpha$  by  $\tau$ , with  $\tau$  the time step used to discretize the time derivative  $\partial_t \mathbf{u}$ , gives a scheme that is stable and does not involve the term  $\chi \mathbf{u}$  on the left-hand side.

The system (7) is approximated in time by using a pressure-correction method. For any time-dependent function  $v(t)$ , we denote by  $v^n$  the approximation of  $v$  at time  $t_n = n\tau$ . The velocity is updated by using the following time-stepping scheme:

$$\begin{aligned} \frac{3\mathbf{u}^{n+1}}{2\tau} - \frac{1}{Re} \Delta \mathbf{u}^{n+1} &= -\nabla p^n + (1 - \chi^{n+1}) \frac{3\mathbf{u}_{\text{obst}}^{n+1}}{2\tau} \\ &+ \chi^{n+1} \left( \frac{4\mathbf{u}^n - \mathbf{u}^{n-1}}{2\tau} - \nabla \left( \frac{4\psi^n - \psi^{n-1}}{3} \right) \right) \\ &+ \chi^{n+1} \left( -(\nabla \times \mathbf{u}^{*,n+1}) \times \mathbf{u}^{*,n+1} + \mathbf{f}^{n+1} \right), \end{aligned} \quad (8)$$

where  $\mathbf{u}^{*,n+1} = 2\mathbf{u}^n - \mathbf{u}^{n-1}$ . Then, the pressure increment  $\psi^{n+1}$  is obtained by solving the following Poisson problem:

$$\Delta \psi^{n+1} = \frac{3}{2\tau} \nabla \cdot \mathbf{u}^{n+1}. \quad (9)$$

Finally, the pressure is updated as follows:

$$p^{n+1} = p^n + \psi^{n+1} - \frac{1}{Re} \nabla \cdot \mathbf{u}^{n+1}. \quad (10)$$

**Table 1**

$L^2$ -norm of the errors on the velocity and outer pressure at time  $t = 0.1$  and rates of convergence. The mesh size  $h$  is set to  $5 \times 10^{-3}$  in  $\mathbb{P}_2$ .

time step $\tau$	$\mathbf{u}$ ( $L^2$ -error)	rate	$p$ ( $L^2$ -error)	rate
$10^{-3}$	6.16E-3	-	8.55E-3	-
$5 \times 10^{-4}$	4.40E-3	0.49	6.10E-3	0.49
$2.5 \times 10^{-4}$	3.14E-3	0.49	4.36E-3	0.48
$10^{-4}$	1.90E-3	0.55	2.64E-3	0.55
$5 \times 10^{-5}$	1.12E-3	0.76	1.51E-3	0.81

The adaptation of the pseudo-penalty technique to pressure-correction methods relies on the observation that the pressure increment  $\psi$  also needs to be penalized by the function  $\chi$  in (8) to get a stable scheme. A proof of the stability of the algorithm with  $u_{\text{obs}} = 0$  is established in [20].

Notice that the velocity and the pressure are solutions of the Navier-Stokes equations in the region where  $\chi = 1$ , i.e., in the fluid domain  $\Omega_{\text{fluid}}(t)$ . In the region where  $\chi = 0$ , i.e., in  $\Omega_{\text{solid}}(t)$ , the momentum equation reduces to  $\frac{3\mathbf{u}^{n+1}}{2\tau} - \frac{1}{R_e} \Delta \mathbf{u}^{n+1} = -\nabla p^n + \frac{3\mathbf{u}_{\text{obs}}^{n+1}}{2\tau}$ ; to first order in  $\tau$ , the solution to this linear Stokes problem is  $\mathbf{u} = \mathbf{u}_{\text{obs}} + \mathcal{O}(\frac{\tau}{R_e})$ . The presence of a boundary layer of thickness  $\mathcal{O}((\frac{\tau}{R_e})^{\frac{1}{2}})$  near the solid-fluid interface limits the global convergence rate in time to  $\frac{1}{2}$ , but when the Reynolds number is large enough the convergence rate in time becomes  $\frac{3}{2}$  as the time step  $\tau$  scales like  $R_e^{-1/2}$ , see Section 1. So the higher the kinetic Reynolds number the smaller the term  $\frac{\tau}{R_e}$ , i.e., the more accurate the method. Another method was used in [3,21,22] based on the direct-forcing approach proposed by [23] where boundary body forces allow the imposition of boundary conditions on interfaces not coinciding with the computational grid.

### 3.3. Manufactured tests

To illustrate the convergence properties of the algorithm, we consider a set of manufactured solutions  $(\chi, \mathbf{u}, p)$  with a relative small Reynolds number  $R_e = 100$ . The domain of computation  $\Omega$  is set to  $\{(r, \theta, z) \mid 0.2 \leq r \leq 1; 0 \leq \theta \leq 2\pi; -1 \leq z \leq 1\}$  and the solutions considered are defined as follows:

$$\begin{cases} \chi(r, \theta, z, t) = \mathbf{1}_{r \geq 0.5}, \\ \mathbf{u}_r(r, \theta, z, t) = (2r - 1)^2 \sin(z + t) \mathbf{1}_{r \geq 0.5}, \\ \mathbf{u}_\theta(r, \theta, z, t) = 0, \\ \mathbf{u}_z(r, \theta, z, t) = (2 - \frac{1}{r})(6r - 1) \cos(z + t) \mathbf{1}_{r \geq 0.5} \\ \quad + (r - 0.5) \sin(2\theta) \mathbf{1}_{r \geq 0.5}, \\ p(r, \theta, z, t) = r^2 z^3 \cos(t) + r \cos(\theta), \end{cases} \quad (11)$$

The source term  $\mathbf{f}$  in the momentum Eq. (8) is computed accordingly. It involves the first five Fourier modes, meaning  $M = 4$  with  $M$  defined in Eq. (4).

To investigate the convergence properties of the algorithm, we perform two sets of tests. First we focus on the time convergence of the method by analyzing results obtained with a fixed mesh size  $h$  equal to  $5 \times 10^{-3}$ . Then we study the global convergence of the algorithm by setting  $\tau = 0.4h^2$  and by performing tests on five different grids of mesh size  $h \in \{0.05, 0.025, 0.0125, 0.005, 0.0025\}$ . The tests are performed using  $M = 4$ , meaning that only the Fourier modes  $m \in \{0, 1, 2, 3, 4\}$  are computed.

Table 1 displays the  $L^2$ -norm of the error on the velocity and the  $L^2$ -norm of the error on the pressure with a fixed mesh size and time step  $\tau \in \{10^{-3}, 5 \times 10^{-4}, 2.5 \times 10^{-4}, 10^{-4}, 5 \times 10^{-5}\}$ . The observed convergence rate is larger than or equal to  $\frac{1}{2}$  which is expected since the Reynolds number is not large ( $R_e = 100$ ). The results shown in Table 2 are performed with  $\tau = 0.4h^2$ . As the error is dominated by the time error, which is of order  $\frac{1}{2}$ , we ex-

**Table 2**

$L^2$ -norm of the errors on the velocity and outer pressure at time  $t = 0.1$  and rates of convergence. The time step is set to  $0.4h^2$  with  $h$  the mesh size in  $\mathbb{P}_2$ .

mesh size $h$	$\mathbf{u}$ ( $L^2$ -error)	rate	$p$ ( $L^2$ -error)	rate
0.05	1.91E-2	-	3.05E-2	-
0.025	1.23E-2	0.63	1.72E-2	0.83
0.0125	5.67E-3	1.12	8.10E-3	1.09
0.005	2.51E-3	0.89	3.45E-3	1.23
0.0025	5.31E-4	2.24	6.14E-4	2.49

pect the global convergence rate to be equal to 1. Indeed, the displayed  $L^2$ -norms of the error on velocity and  $L^2$ -norm of the error on the pressure are compatible with the rate  $\mathcal{O}(h)$ . We note that the method has also been validated in [20] against classical test cases such as the flow past a sphere at various Reynolds numbers.

### 3.4. LES Scheme: Entropy viscosity stabilization

To avoid the accumulation of energy at the grid scale at high Reynolds numbers when the grid is not fine enough to resolve the Kolmogorov scale, we use a LES-like technique called entropy viscosity. This method, developed in [24–26], consists of adding a local artificial viscosity made proportional to the residual of the kinetic energy balance. This artificial viscosity is added on the right-hand side of (7a) in the form  $\nabla \cdot (\nu_E \nabla \mathbf{u})$ . This induces a nonlinear diffusion proportional to the local energy imbalance that in turn allows the unresolved scales to be better accounted for. The method has its roots in the notion of suitable weak solutions introduced by [27] and which has been shown by [28] to be the only reasonable notion of solution currently available for the 3D Navier-Stokes equations.

We now give some technical details on the computation of the entropy viscosity. Since the approximation mixes finite elements and Fourier approximation, we construct a three-dimensional mesh by considering the tensor product of the finite element mesh in the meridian section with the uniform azimuthal one-dimensional mesh induced by the Fourier approximation. Denoting by  $M$  the number of complex azimuthal Fourier modes, the mesh size in the azimuthal direction at the radius  $r$  is  $2\pi r / (2M - 1)$ . For each two-dimensional finite element cells  $K$ , we denote by  $h_K = \min(\min_{\mathbf{x} \in K} \frac{2\pi r}{2M - 1}, \text{diam}(K))$ . Assuming that  $n \geq 2$ , we define the residual of the momentum equation as follows:

$$\text{Res}_{\text{NS}}^n = \frac{\mathbf{u}^n - \mathbf{u}^{n-2}}{2\tau} + (\mathbf{u}^{n-1} \cdot \nabla) \mathbf{u}^{n-1} - \frac{1}{R_e} \Delta \mathbf{u}^{n-1} + \nabla p^{n-1} - \mathbf{f}^{n-1}. \quad (12)$$

This residual is then computed at each time step and over every mesh cell in the real space. The local artificial viscosity is defined on each cell  $K$  by:

$$\nu_{R|K}^n = \frac{h_K^2 \|\text{Res}_{\text{NS}}^n \cdot \mathbf{u}^n\|_{L^\infty(D_K)}}{\|\mathbf{u}^n\|_{L^\infty(D_K)}}. \quad (13)$$

where  $D_K$  is the patch composed of the cells sharing one face with the cell  $K$  in the real space. The quantity  $\nu_{R|K}^n$  is expected to be as small as the consistency error in smooth regions and to be large in the regions where the Navier-Stokes equations are not well resolved. To be able to run with CFL numbers of order  $\mathcal{O}(1)$ , we finally define the entropy viscosity as follows:

$$\nu_{E|K}^n = \min(c_{\text{max}} h_K \|\mathbf{u}^n\|_{L^\infty(D_K)}, c_e \nu_{R|K}^n), \quad (14)$$

where  $c_{\text{max}} = \frac{1}{8}$  and  $c_e$  is a tunable constant  $\mathcal{O}(1)$ . In the following we set  $c_e = 1$ . Thus defined, and given that we use  $\mathbb{P}_2$  polynomials to approximate the velocity, the entropy viscosity scales like  $\mathcal{O}(h_K^3)$

in smooth regions and scales like  $\mathcal{O}(h_K)$  in regions with very large gradients.

This LES technique has been validated with  $c_{\max} = \frac{1}{8}$  and  $c_e = 1$  in [29] for flows in precessing cylinders and in [30] for turbulent flows in a flexible pipe (notice that the parameter  $\alpha$ , defined therein in equation (2.13), is equal to  $c_e/2$ ). We have used this method in [31] to perform high Reynolds number computations in a magnetohydrodynamics version of the von Kármán experiment.

#### 4. Tools and flow description

We describe in this section the different diagnostic tools, the von Kármán flow, the experimental setup and the numerical parameters that we use.

##### 4.1. Diagnostic tools

###### 4.1.1. Time averages

Since we are going to regularly invoke time averages, for any time dependent quantity  $A : [0, T] \rightarrow \mathbb{R}^n$  we define:

$$\langle A \rangle = \frac{1}{T} \int_0^T A(\tau) d\tau. \quad (15)$$

Moreover, given an experimental time series  $(A_k)_{1 \leq k \leq N}$  measured at a fixed point in the inertial frame of reference of the laboratory, we define the inertial discrete time average as follows:

$$\langle A \rangle_{\circ} = \frac{1}{N} \sum_{k=1}^N A_k. \quad (16)$$

Notice that when the flow is time-dependent this definition implies averaging the characteristics of the quantity  $A$  not only in time but also with respect to the azimuth. Using the cylindrical coordinates  $(r, \theta, z)$ , this corresponds to extracting the time average of the angular Fourier mode  $m = 0$  of  $A(r, \theta, z, t)$ .

###### 4.1.2. Energy dissipation and torque

The power that is injected inside the VK flow and that is eventually transformed into heat by viscous effects can be estimated from the two torques  $C_1$  and  $C_2$  that are exerted on the top and the bottom impellers, respectively; the injected power in question is given by the expression  $P_{\text{inj}} = 2\pi f_i (|C_1| + |C_2|)$ . In the statistically stationary regime, the mean input power equals the mean dissipation power. A useful diagnostic of the dissipation power can then be derived using a non-dimensional number  $P^*$  as follows:

$$P^* = \frac{\langle P_{\text{inj}} \rangle}{2\rho R^5 (2\pi f_i)^3}, \quad (17)$$

where we recall that  $\rho$  is the density of the fluid. A non-dimensionalized torque can also be defined as

$$K_p = \frac{\langle |C_1| + |C_2| \rangle}{2\rho R^5 (2\pi f_i)^2}. \quad (18)$$

Notice that  $K_p = P^*$ .

In the experiment, the torque measurements at each impeller are performed using either the engines or torque meters. The torque applied to the top shaft is denoted  $C_1$ , and the torque applied to the bottom shaft is denoted  $C_2$ . Following the procedure described in [32], the torques are calibrated using measurements at different mean frequencies, so as to remove spurious contributions from genuine offsets or mechanical frictions. The torque measurements give the power dissipation.

Numerically, we can compute the dimensionless torque  $K_p$  as follows:

$$K_p = \frac{1}{2} \int_{\Omega_{\text{solid}}} |(\mathbf{r} \times \mathbf{f}_s) \cdot \mathbf{e}_z| d\Omega, \quad (19)$$

where  $\mathbf{f}_s$  is the non-dimensional body force that induces the solid rotation of the impellers. The force  $\mathbf{f}_s$  can be written as  $\nabla \cdot (p\mathcal{I} - R_e^{-1} \nabla \mathbf{u})$ , where  $\mathbf{u}$  and  $p$  are any smooth extensions of the velocity and the pressure in the solid. Notice that the term  $\mathbf{f}_s$  and the source term  $\mathbf{f}$  in the Navier-Stokes Eq. (1) are unrelated. In the sequel  $\mathbf{f}$  is set to zero. The fluid is driven by the movement of the counter-rotating impellers, represented by the pseudo-penalty method, and not by an exterior forcing  $\mathbf{f}$ . Using the notation from (5) and (6), we deduce from the expression of the discrete momentum balance (8) that the torque at time  $t_{n+1}$  is given by

$$K_p = \frac{3}{4} \int_{\Omega} r(1 - \chi) \text{sgn}(f_2 z) \frac{\mathbf{u}^{n+1} - \mathbf{u}_{\text{obst}}}{\tau} \cdot \mathbf{e}_{\theta} d\Omega, \quad (20)$$

where  $\text{sgn}$  is the sign function introduced in (6).

##### 4.2. The von Kármán flow

###### 4.2.1. Symmetries

When the two impellers counter-rotate at the same frequency, i.e., when  $f_1 = -f_2$ , the VK setup is symmetric with respect to any rotation of angle  $\pi$  about any axis in the equatorial plane that crosses the rotation axis. This type of symmetry is henceforth referred to as  $\mathcal{R}_{\pi}$ -symmetry [33], and acts as follows in cylindrical coordinates:

$$\mathcal{R}_{\pi} \begin{pmatrix} u_r \\ u_{\theta} \\ u_z \end{pmatrix} (r, \theta, z) \equiv \begin{pmatrix} u_r \\ -u_{\theta} \\ -u_z \end{pmatrix} (r, -\theta, -z) \quad (21)$$

In the absence of blades on the supporting disks, the setup is also axisymmetric. At very low Reynolds numbers, the instantaneous velocity field obeys these symmetries. At large Reynolds numbers, the time averaged velocity is statistically axisymmetric but can experience breaking of the  $\mathcal{R}_{\pi}$ -symmetry in certain conditions as we will report below.

###### 4.2.2. Mean flow topology

The topology of the time-averaged and azimuthally-averaged mean flow (in short mean flow) is simple and depends on whether the forcing conditions are CONTRA or ANTI:

1. The CONTRA mean flow is divided into two toroidal recirculation cells separated by an azimuthal shear layer. In a vertical plane containing the axis of rotation, the corresponding mean velocity field is symmetric under  $\mathcal{R}_{\pi}$  (i.e.,  $\langle u_r(r, -z) \rangle = \langle u_r(r, z) \rangle$ ,  $\langle u_{\theta}(r, -z) \rangle = -\langle u_{\theta}(r, z) \rangle$ ,  $\langle u_z(r, -z) \rangle = -\langle u_z(r, z) \rangle$ ) and there is a strong shear layer in the middle.
2. The ANTI mean flow has two possible geometries depending on the Reynolds number and the shape of the impellers. (1) The flow can have the same geometric symmetries as the CONTRA mean flow. (2) The flow can have a bifurcated geometry resulting from the merging of the two toroidal counter-rotating recirculation cells into a single cell (see [7] and [8]). In this case, the mean velocity field in any vertical plane containing the axis of rotation is no longer invariant under  $\mathcal{R}_{\pi}$ . The mean flow is then mainly composed of one cell in the vertical direction with a strong shear layer at the impeller that rotates in the direction opposite to the orthoradial mean flow. This bifurcated state only exists for Reynolds numbers that are large enough (see [7]) and for impellers that are fitted with blades that are sufficiently curved, which is the case of the TM87 impellers studied in the present paper. This turbulent bifurcation results in multistability between the two turbulent flow states, with possible complex dynamics between them (see [34–36]). It is therefore a genuine challenge to reproduce numerically this configuration.

**Table 3**

Experimental parameters: kinetic Reynolds number  $R_e$ , flow type, kinematic viscosity  $\nu$ , rotation frequency  $f$ .

$R_e$	$10^2$	$10^3$	$3 \times 10^5$	$3 \times 10^5$	$3 \times 10^5$
Flow type	CONTRA	CONTRA	CONTRA	ANTI symmetric	ANTI bifurcated
$\nu$ (m <sup>2</sup> s <sup>-1</sup> )	$4.3 \times 10^{-4}$	$4.3 \times 10^{-4}$	$1.0 \times 10^{-6}$	$1.0 \times 10^{-6}$	$1.0 \times 10^{-6}$
$f$ (Hz)	0.68	6.8	5.0	5.0	5.0

**Table 4**

Numerical parameters for the computations: kinetic Reynolds number  $R_e$ , flow type, numerical model DNS or LES, timestep  $\tau$ , mesh size in the blade region  $h_{\min}$ , mesh size at the outer boundary  $h_{\max}$  (the meridian mesh is non-uniform), number of grid points in the  $\mathbb{P}_2$  meridian mesh  $n_{df}$ , number of real Fourier modes, number of processors.

$R_e$	$10^2$	$10^3$	$10^5$	$10^5$	$10^5$
Flow type	CONTRA	CONTRA	CONTRA	ANTI symmetric	ANTI bifurcated
Model	DNS	DNS	LES	LES	LES
$\tau$	$2.5 \times 10^{-3}$	$2.5 \times 10^{-3}$	$1.25 \times 10^{-3}$	$1.25 \times 10^{-3}$	$10^{-4}$
$h_{\min}$	$2 \times 10^{-2}$	$5 \times 10^{-3}$	$5 \times 10^{-3}$	$5 \times 10^{-3}$	$2.5 \times 10^{-3}$
$h_{\max}$	$2 \times 10^{-2}$	$10^{-2}$	$2 \times 10^{-2}$	$2 \times 10^{-2}$	$10^{-2}$
$n_{df}$	7589	65,861	46,291	46,291	193,051
modes	128	128	128	128	512
nprocs	128	128	128	128	2048

### 4.3. Experimental implementation

#### 4.3.1. Experimental setup

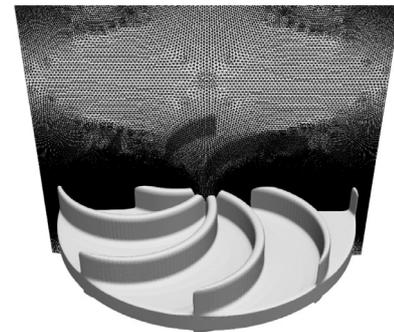
The VK experimental setup used for the present study has been thoroughly described in [7–10]. The fluid is confined inside a cylinder of radius  $R = 100$ mm, and put in motion by two rotating impellers of radius 92.5mm (see Fig. 1 and Fig. 2). We recall that the lengths are non-dimensionalized with respect to the radius of the cylinder,  $R$ . The aspect ratio of the experiment is defined as the (non-dimensional) distance between the inner faces of the two disks supporting the blades,  $H = 1.8$ . The turbulence properties (anisotropy, fluctuations, dissipation) are influenced by the geometry of the impellers, their non dimensional radius  $R_t$ , the oriented angle  $\alpha$  (see Fig. 2) and height  $h_b$  of the blades, and the number  $n$  of blades [37]. In the present paper, we consider mainly TM87 impellers, with  $n = 8$  blades,  $h_b = 0.2$ ,  $|\alpha| = 72^\circ$  and  $R_t = 0.925$ . Mixtures of water and glycerol with different dilution rates are used to change the viscosity of the fluid. The temperature is maintained constant by means of heat exchangers. A summary of the experimental cases presented in this paper is given in Table 3.

Both the torques and the mean flow topology are very sensitive to geometric parameters like the height and the curvature of the blades, the radius of the impellers, the aspect ratio, as discussed in [9,32,37–39]. Therefore to be able to reproduce numerically the experiments, we have observed that it is essential that the geometry of the setup be reproduced as accurately as possible in SFE-MaNS.

#### 4.3.2. Multi-scale velocity measurements

The velocity measurements used in the present paper result from two types of techniques: (i) Stereoscopic Particle Image Velocimetry (SPIV) and (ii) Laser Doppler Velocimetry measurements (LDV).

The SPIV system provides the three components of the velocity field in a meridian plane on a grid of typical size  $90 \times 70$  points. The optical device can be adapted so that the horizontal and the vertical distance between two measurement points can be controlled in the range  $[2.4 \times 10^{-3}, 2.4 \times 10^{-2}]$ . The meridian section that can be explored is  $\{(r, z) \in [0, 1] \times [-0.75, 0.75]\}$ . The time series



**Fig. 3.** Shape of the impellers and the computational grid in  $(r,z)$  plane with 128 Fourier modes,  $h_{\max} = 2 \times 10^{-2}$  and  $h_{\min} = 5 \times 10^{-3}$ .

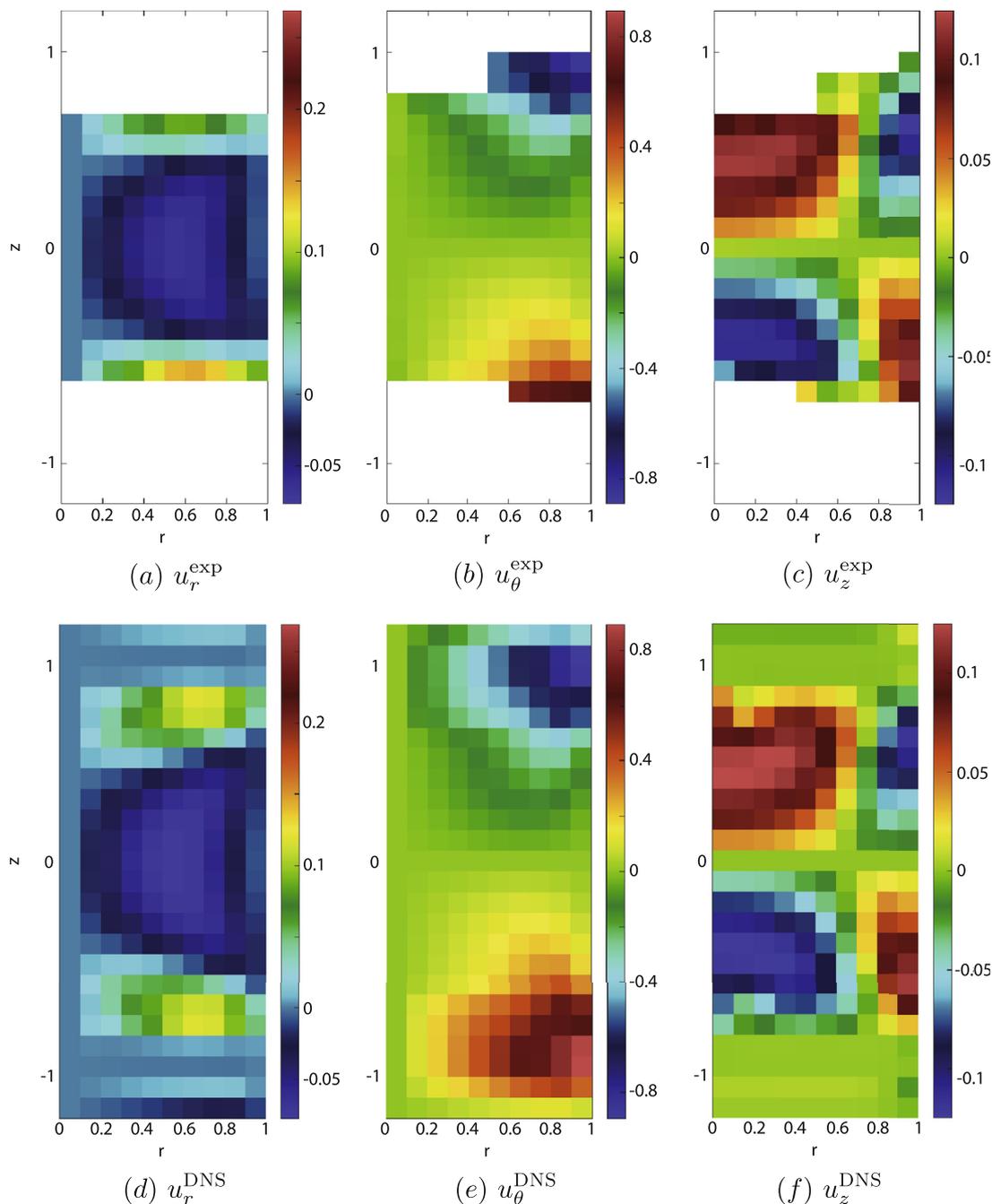
are composed of about 3000 to 30000 frames regularly sampled at 15Hz. The time average of time series of SPIV measurements is denoted  $\langle \cdot \rangle_t$ , see (16). Because of the constraints on the measurements technique and the unsteadiness of the velocity pattern, such time-average automatically produces an *azimuthal* average, i.e., time averaging projects the measurements onto the angular Fourier mode  $m = 0$ .

We have also performed a few Laser Doppler Velocimetry measurements. These measurements provide the mean azimuthal and mean vertical components of the velocity in a meridian plane on a grid composed of  $11 \times 17$  points located at  $0 \leq r \leq 10\Delta r$  with  $\Delta r = 0.1$  and  $-8\Delta z \leq z \leq 8\Delta z$  with  $\Delta z = 0.1125$ .

### 4.4. Summary of the numerical parameters

The numerical parameters that have been used in the various simulations reported in this paper are listed in Table 4. The computations are done only in the TM87 configuration.

The spatial resolution in the meridian plane and in azimuth of DNS simulations is set to match the Reynolds number, i.e., the computational grid is refined as  $R_e$  increases. The meshes are usually coarser for LES runs than for DNS runs. Fine meshes are used to simulate the ANTI bifurcated flow since very thin shear layers



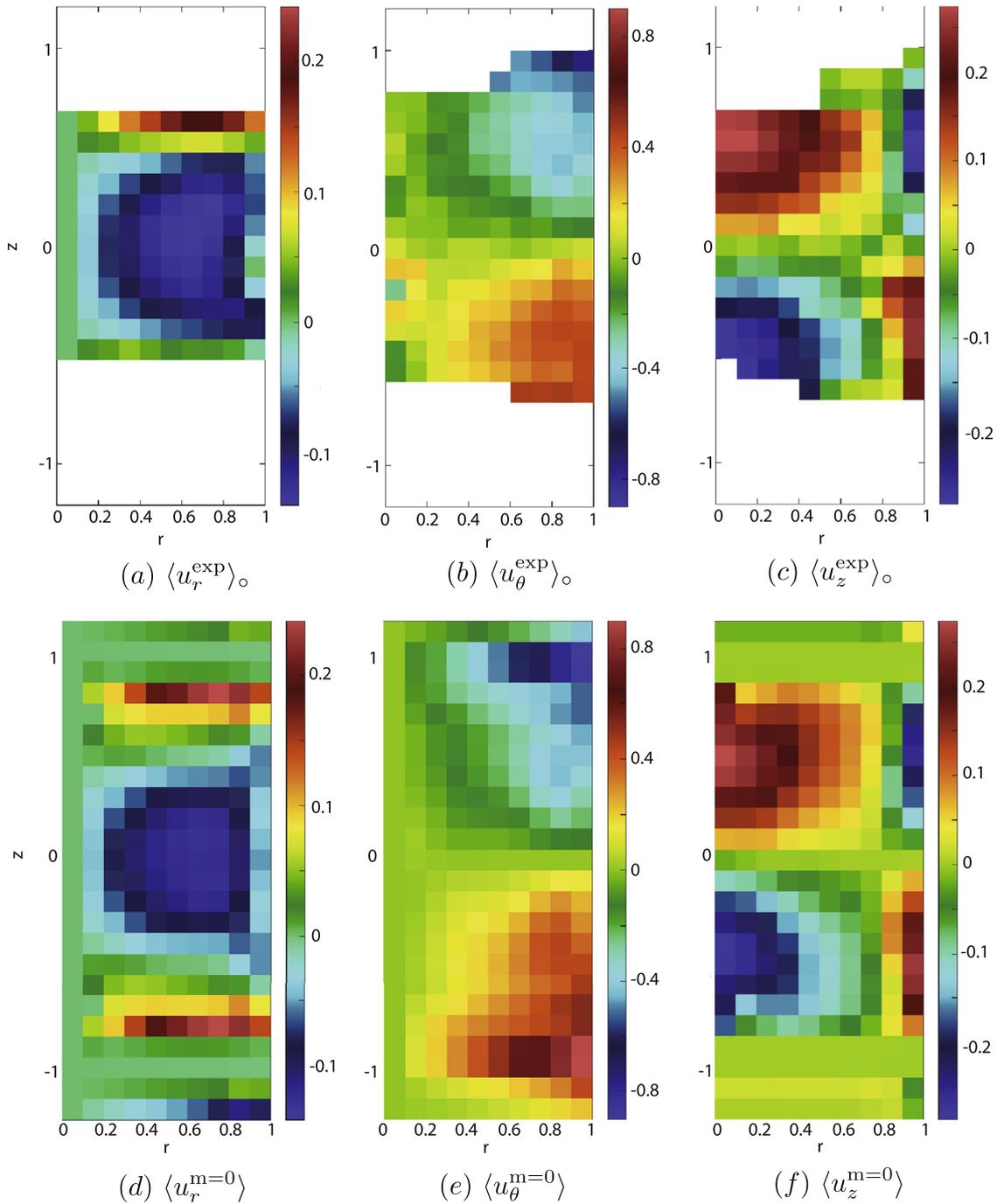
**Fig. 4.** Stationary and axisymmetric experimental and DNS velocity field in the CONTRA configuration at  $Re = 10^2$ : (a)-(d) radial component  $u_r$ , (b)-(e) azimuthal component  $u_\theta$ , (c)-(f) vertical component  $u_z$ .

are created in this case (see Fig. 13 (b)-(e) for  $0.6 \leq z \leq 0.8$ ). The mesh sizes  $h_{\min}$  and  $h_{\max}$  in Table 4 are the typical distance between two grid points on the velocity mesh (i.e., the  $\mathbb{P}_2$  mesh). Between 128 to 512 real Fourier modes are typically used. The shape of the impellers and a computational grid are displayed in Fig. 3. The parallelization is done with one complex Fourier mode per processor, and the meridian plane is further divided among the processors by using a domain decomposition technique, the graph partitioning being done by METIS. The linear algebra in the meridian section is handled by PETSc and the fast Fourier transforms are done with FFTW3. Depending on the spatial resolution and the Reynolds number, one rotation period (one turn) requires between 2 to 63 wall-clock hours on the cluster IBM x3750-M4 from GENCI-IDRIS. Each run does between 15 to 60 turns. The cumulated com-

puting time for the runs presented in this article is about  $7 \times 10^5$  CPU hours on one processor.

### 5. Comparisons experiment vs. numerics

In this section we compare experimental and numerical velocity profiles in a meridian section of the cylindrical container at various Reynolds numbers and in different operating conditions. The comparisons are done on snapshots and on the time-averaged velocity fields. In order to have good quantitative comparisons, we always use the same colorbars for the experimental data and the numerical results. At the end of the section we also compare torque measurements with computations over a wide range of Reynolds numbers.



**Fig. 5.** Time-averaged experimental and DNS velocity field ( $m = 0$ ) in the CONTRA configuration at  $Re = 10^3$ : (a)-(d) radial component  $u_r$ , (b)-(e) azimuthal component  $u_\theta$ , (c)-(f) vertical component  $u_z$ .

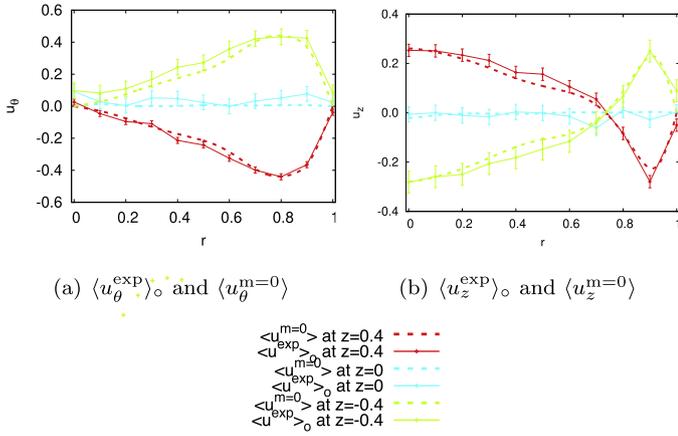
### 5.1. Flow topology at low Reynolds numbers

We start by investigating the VK flow at low Reynolds numbers; i.e.,  $Re \leq 10^3$ .

#### 5.1.1. Low Reynolds numbers: Steady-state regime

At very low Reynolds numbers (ie  $Re < 5 \times 10^2$ ), the velocity field is stationary. Moreover, the CONTRA and the ANTI operating conditions give very similar results. Therefore we do not show the two cases but rather focus on the CONTRA operating mode. We show in Fig. 4 the three components of the stationary and axisymmetric velocity field at  $Re = 10^2$  using the cylindrical coordinate

representation. We compare in panels (a) and (b) the experimental measurements of the radial component of the velocity with the computational results. The comparisons for the azimuthal component are shown in panels (c) and (d). The comparisons for the axial component are shown in panels (e) and (f). The white zones in the experimental fields correspond to areas where measurements were not possible due to the presence of the blades. The resolution of the LDV measurements being much lower than the numerical results, we have interpolated the numerical data on large pixels corresponding to the experimental resolution. This process allows for a better comparison between the experiments and the numerical simulations. Fig. 4 shows that the numerical data and the experi-



**Fig. 6.** Radial profiles of  $u_\theta$  and  $u_z$  for time-averaged experimental and DNS velocity field ( $m=0$ ) in the CONTRA configuration at  $Re = 10^3$ :  $\langle u^{\text{exp}} \rangle_\circ$  in solid line with error bars,  $\langle u^{m=0} \rangle$  in dashed line at various  $z$  as indicated. The color convention applies to all the profiles in other figures.

mental results are very similar with slight differences close to the border of the experimental acquisition zone.

### 5.1.2. Low Reynolds numbers: Time-dependent regime

The flow becomes time-dependent at  $Re = 500$ . We compare in Fig. 5 the experimental and the numerical time-averaged velocity fields in the CONTRA configuration at  $Re = 10^3$  using the same pixelization procedure as described above. Notice that this time we use the averaging operator  $\langle \cdot \rangle_\circ$  defined in (16) to average the experimental data in time. For the numerical simulations, the averaging is done in azimuth and in time; that is, we show the time average of the Fourier mode  $m=0$ .

Fig. 6 shows radial profiles of averaged azimuthal and vertical velocity components at  $z \in \{-0.4, 0, 0.4\}$ . For the LDV experimental data, measurements are performed in one meridian section. Since for all  $z \in \mathcal{Z} := \{-0.4, 0, 0.4\}$  the quantities  $u_\theta(r=0, z)$ ,  $u_\theta(r=1, z)$  and  $u_z(r=1, z)$  must be equal to zero, we estimate the experimental error on  $u_\theta$  at  $z \in \mathcal{Z}$  as follows:  $\Delta_\theta(z) := \max\{|u_\theta^{\text{exp}}(r=0, z)|, |u_\theta^{\text{exp}}(r=1, z)|\}$  and the error on  $u_z$  at  $z \in \mathcal{Z}$  is  $\Delta_z(z) := |u_z^{\text{exp}}(r=1, z)|$ . Our experience is that this estimate of the experimental error is a better alternative to using the variance of the temporal signals since the temporal signals are short.

The agreement between the numerical profiles and the experimental profiles is within the experimental errors. While the DNS profiles are exactly symmetric with respect to  $z$ , the experimental data are coarse and only approximately symmetric. In any case the comparison is satisfactory: the local maximum of  $|u_\theta|$  is located at  $r \approx 0.8$  for  $z = \pm 0.4$ ; the change of sign of  $u_z$  for  $z = \pm 0.4$  occurs at  $r \approx 0.75$ .

We now compare the CONTRA and the ANTI regimes at  $Re = 10^3$ . In Fig. 7 we compare the numerical results obtained in the CONTRA operating configuration with the numerical results obtained in the ANTI operating configuration. The flow patterns look different. Close to the blades, the radial centrifugal component of the velocity in the CONTRA case is stronger than in the ANTI configuration, but in the equatorial shear layer the radial velocity component is more intense and focused in the ANTI regime. Note also that the azimuthal component of the velocity is overall stronger in the ANTI than in the CONTRA regime. These features persist at larger Reynolds numbers for the averaged velocities.

## 5.2. Flow topology at high Reynolds numbers

We now describe the flow topology at high Reynolds numbers. The experimental data reported below have been obtained at  $Re = 3 \times 10^5$  and the LES computations have been done at  $Re = 10^5$ . Therefore the comparisons are performed at slightly different Reynolds numbers. At these Reynolds numbers, the CONTRA configuration gives a solution that is highly turbulent but on average the flow is organized into two cells that are invariant under the  $\mathcal{R}_\pi$  transformation. This structure is very robust with respect to the preparation of the flow. This is not the case for the ANTI configuration. The flow is also highly turbulent in this operating mode, but, depending on the preparation of the flow, one observes two possible time-averaged states. One state is composed of two cells as in the CONTRA operating conditions, but the other one is composed of one cell only. We have observed this bifurcation to occur in the ANTI configuration at  $Re \sim 10^4$  (see Section 5.3 and Fig. 15 for a detailed discussion).

### 5.2.1. CONTRA Operating mode

We start by comparing the results for the CONTRA operating mode. We show in Fig. 8 the time and azimuthally averaged velocity field at  $Re \sim 10^5$ . The simulation has been done by using the final snapshot of a statistically converged simulation at  $Re = 10^4$  as initial data. About 20 turns have been performed at  $Re = 10^5$ .

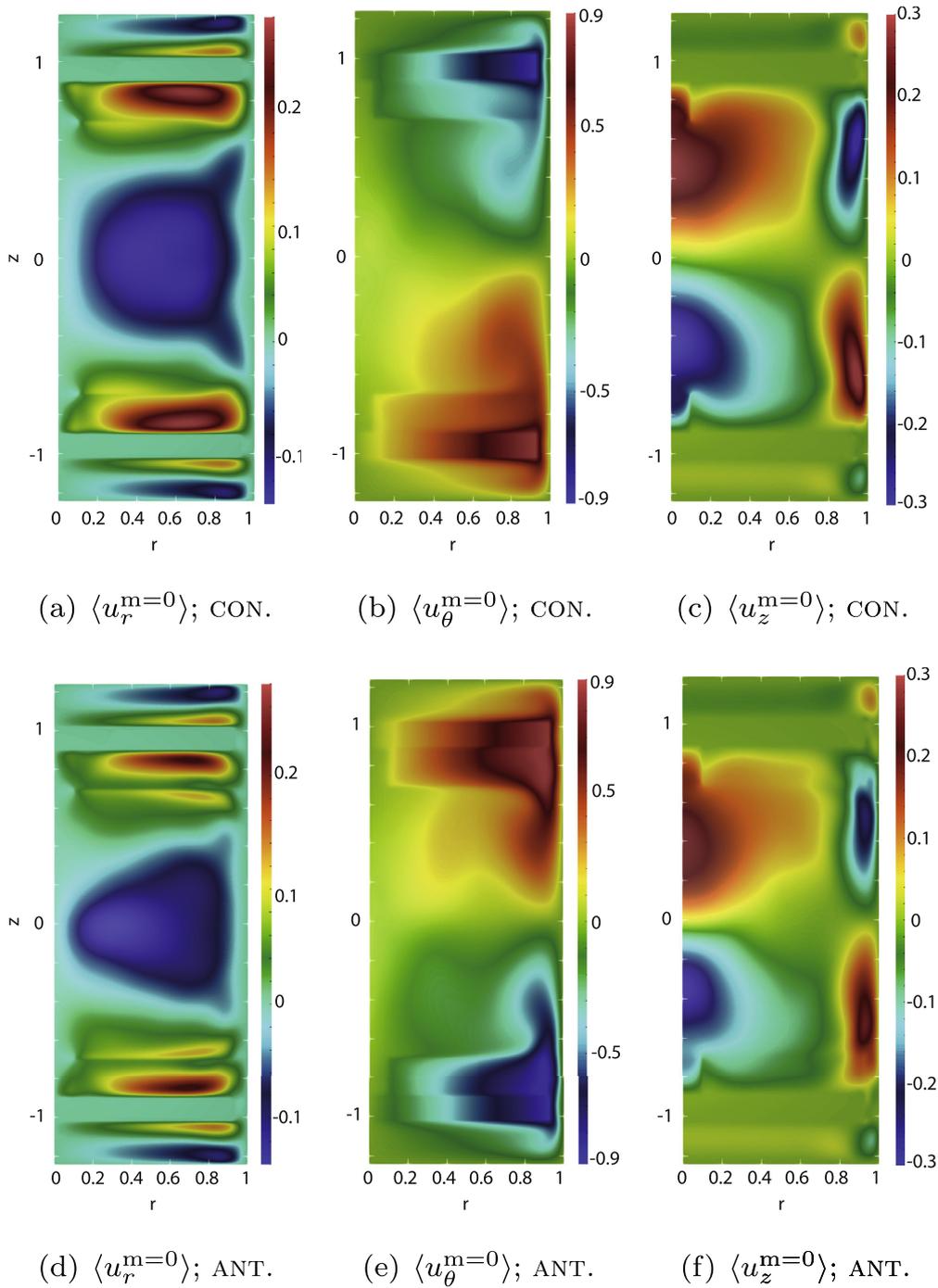
Since the simple time averages over the 20 rotation periods of the LES computations are not long enough to be fully converged statistically, we show in Fig. 8 only the time average of the Fourier mode  $m=0$  of the velocity field. This corresponds to the experimental data mean operator  $\langle \cdot \rangle_\circ$  which only detects the Fourier mode  $m=0$  anyway. Notice that this time the image resolutions are now different; one sees the blades in the numerical simulations but these are not visible in the experiments. The blades start at  $r=0.1$  as shown in Fig. 2. Also the SPIV allows us to reach only  $r=0.95$ . This explains why we see a boundary layer in the LES simulation close to  $r=1$  in panel 8(d) which is not captured by the SPIV measurements in the panel 8(a) (white pixels indicate that there are no experimental data close to the boundary). Fig. 9 shows averaged radial profiles of the azimuthal and the vertical velocity components at  $z \in \{-0.4, 0, 0.4\}$ . For the SPIV experimental data, measurements are performed over an entire meridian plane, i.e., measurements are done simultaneously on two diametrically opposite meridian sections. The quantities displayed are  $u_z^{\text{exp}}(r, z) = \frac{1}{2}(u_z(r, 0, z) + u_z(r, \pi, z))$  and  $u_\theta^{\text{exp}}(r, z) = \frac{1}{2}(u_\theta(r, 0, z) - u_\theta(r, \pi, z))$ . The error bars for each component are the variance of the temporal signals. This estimation of the experimental error is also used in Fig. 12 and Fig. 14. The numerical profiles fit the error bar region of the experimental data. This suggests that the difference in the Reynolds numbers ( $10^5$  for the numerical simulations and  $3 \times 10^5$  for the experiments) has a moderate impact on the average profiles. Furthermore these profiles are similar to the ones obtained at the much smaller  $Re = 10^3$ : the local maximum of  $|u_\theta|$  is around  $r=0.8$  at  $z = \pm 0.4$  and the change of sign of  $u_z$  occurs at  $r \approx 0.75$  for  $z = \pm 0.4$ .

We compare in Fig. 10 experimental and computational snapshots of the Cartesian components of the velocity field in a vertical plane passing through the axis. These figures clearly show that the flow is highly turbulent. Of course, these instantaneous snapshots are not identical but they share similar amplitudes and structures.

### 5.2.2. ANTI Operating mode: Symmetric solution

We now show in Fig. 11 the time-averaged experimental and numerical velocity fields for the ANTI configuration.

Here the experimental flow at  $Re = 3 \times 10^5$  is obtained by progressively increasing the angular frequency of the impellers and making sure that the two angular velocities are all the time exactly

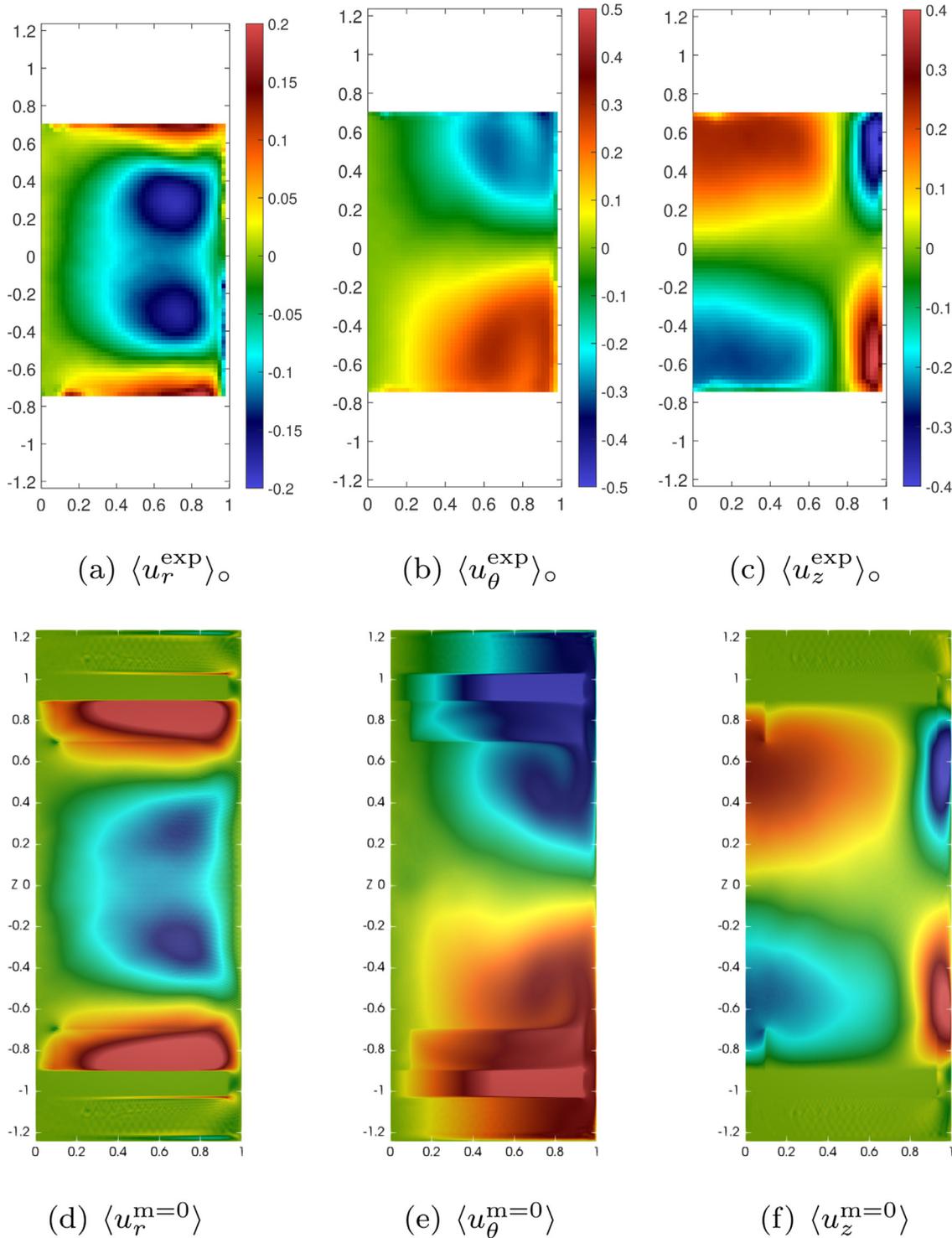


**Fig. 7.** Time-averaged DNS velocity field (Fourier mode  $m = 0$ ) in CONTRA and ANTI operating configurations at  $Re = 10^3$ : (a)-(d) radial component  $u_r$ , (b)-(e) azimuthal component  $u_\theta$ , (c)-(f) vertical component  $u_z$ .

opposite. The preparation of the numerical simulations at  $Re = 10^5$  is also done by progressively increasing the Reynolds number and by always enforcing the two angular velocities to be exactly opposite as explained in Section 5.2.1. This process leads to a highly turbulent flow that is organized on average into two cells that are  $\mathcal{R}_\pi$  symmetric. The organization into two cells is clearly visible in panels 11(c) and (f). Notice, though, that the CONTRA and ANTI mean flow fields are very different. The differences are particularly noticeable when comparing the radial component of the velocity in the panels 8(a) and (d) with that in the panels 11(a) and (d). Also, by comparing the panels 8(b) and (e) with the panels 11(b)

and (e), we observe that the ANTI configuration produces stronger azimuthal components of the velocity than the CONTRA configuration. In the ANTI configuration the large values of the azimuthal component are concentrated near the lateral wall. Notice also that the radial and axial components of the velocity have smaller values than in the CONTRA configuration.

Fig. 12 compares the experimental and numerical profiles for the symmetric ANTI configuration at high Reynolds numbers. Again the agreement is good since the numerical profiles are inside the error bar region of the experimental observations. The azimuthal profiles at  $z = \pm 0.4$  show that the extrema are located at



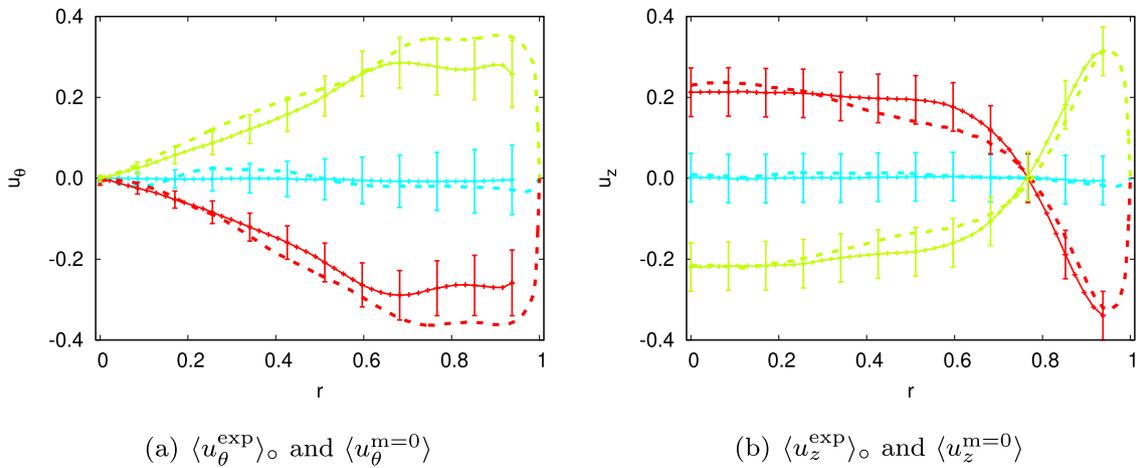
**Fig. 8.** Time and azimuthal averaged velocity field in the CONTRA configuration.  $R_e = 3 \times 10^5$  for the experiments;  $R_e = 10^5$  for the computations: (a)-(d) radial component  $u_r$ , (b)-(e) azimuthal component  $u_\theta$ , (c)-(f) vertical component  $u_z$ .

$r \approx 0.95$  in the boundary layer which the experimental SPIV cannot resolve. The amplitudes of the extrema of  $u_\theta$  are twice those observed in the CONTRA configuration. The change of sign of  $u_z$  still occurs around  $r \approx 0.75$  for  $z = \pm 0.4$ .

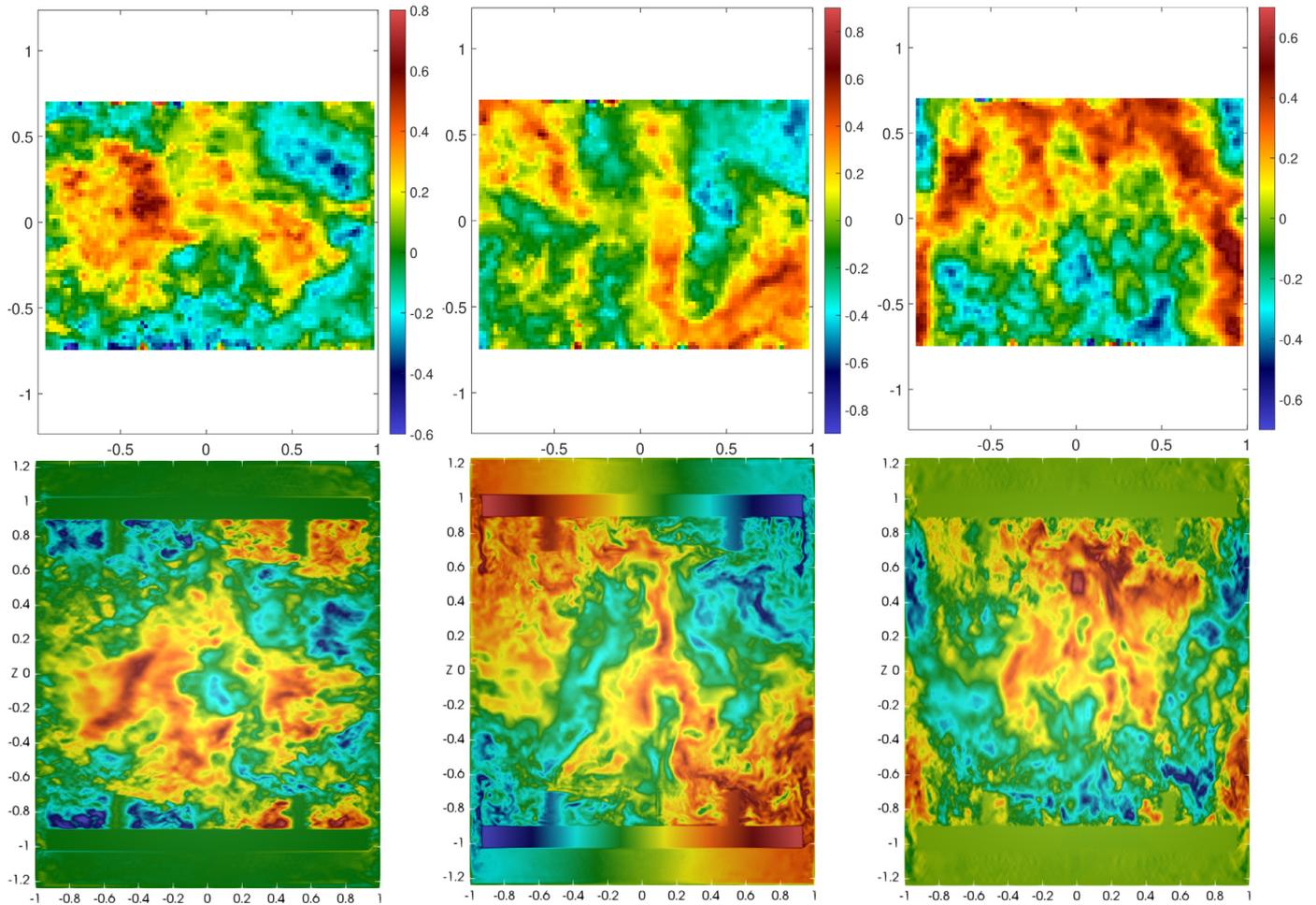
### 5.2.3. ANTI Operating mode: Bifurcated solution

We now focus on the bifurcated flow for the ANTI configuration. This solution is obtained by preparing the flow in a non-

symmetric way. In the experiment, the angular frequencies of the top and the bottom impellers are not increased simultaneously. For some time one of the impellers rotates faster than the other one. Then, eventually, exact counter-rotation is prescribed and maintained. This produces a symmetry breaking that allows the flow to explore another solution branch that is not invariant under  $\mathcal{R}_\pi$ . For the numerical simulations we proceed as follows. We use a snapshot of the ANTI configuration at  $R_e = 10^4$  as initial



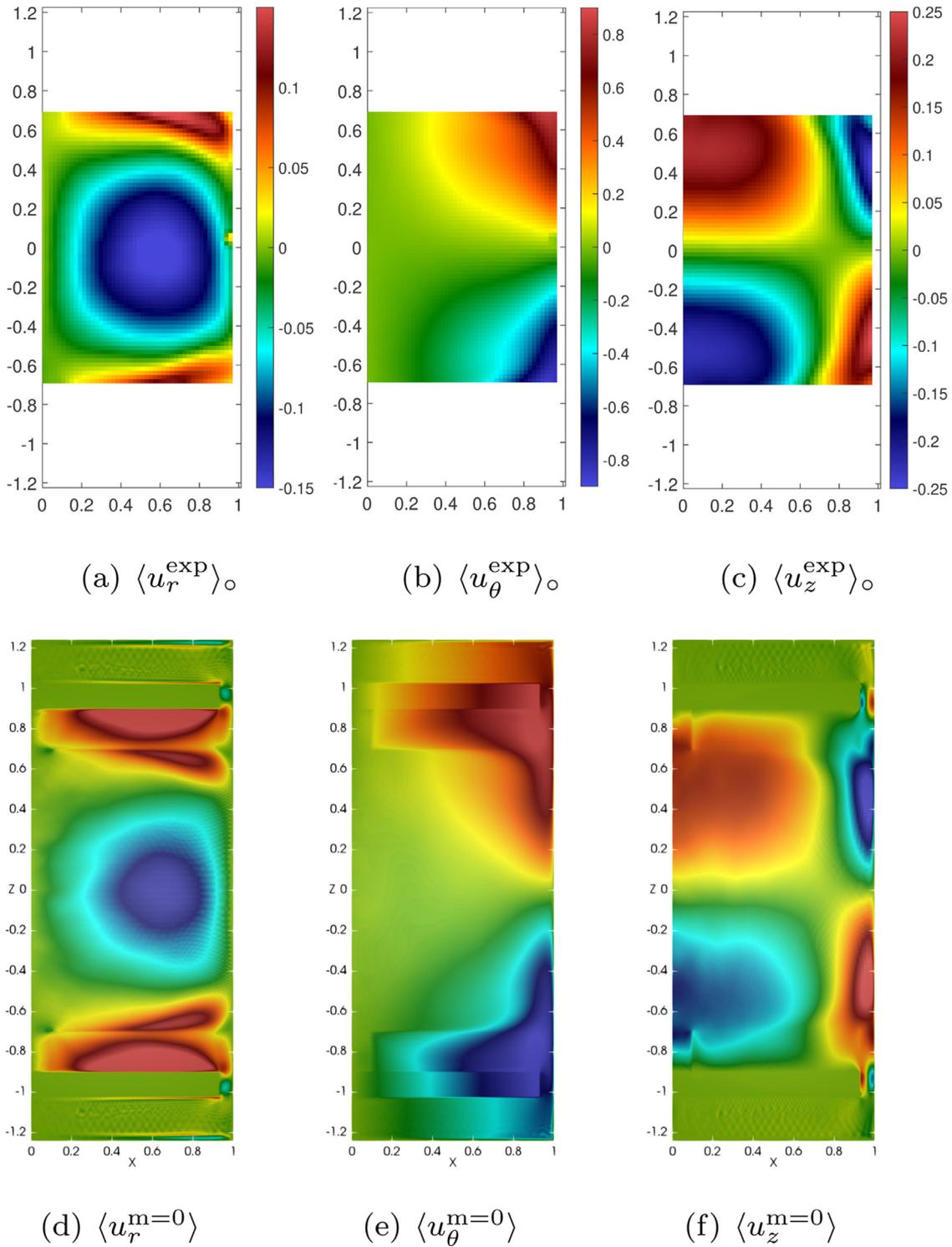
**Fig. 9.** Radial profiles of  $u_{\theta}$  and  $u_z$  for time-averaged experimental and LES velocity fields ( $m=0$ ) in the CONTRA configuration at  $Re = 3 \times 10^5$  for the experiment and  $Re = 10^5$  for the computation:  $\langle u^{\text{exp}} \rangle_{\circ}$  in solid line with errorbars,  $\langle u^{m=0} \rangle$  in dashed line. Color labels are defined in Fig. 6.



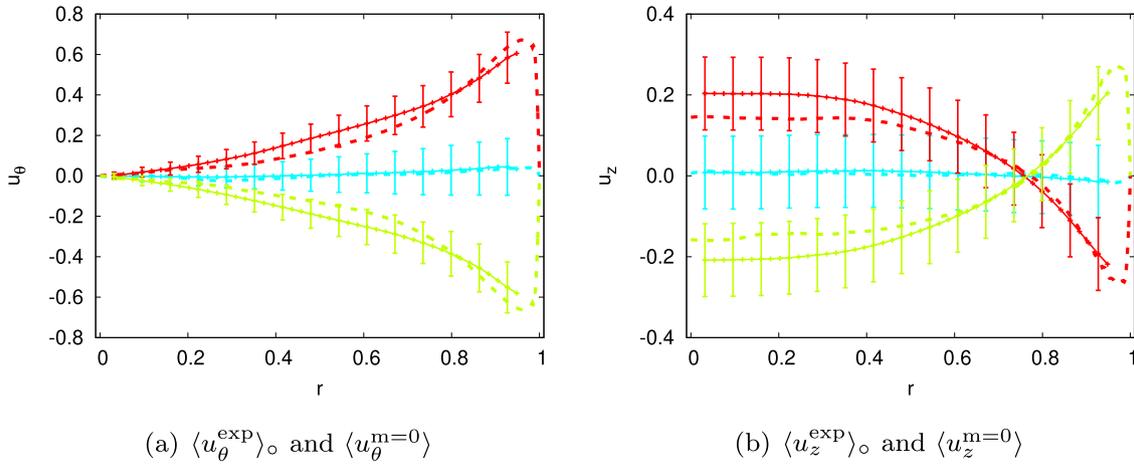
**Fig. 10.** Instantaneous velocity fields in the CONTRA configuration in a vertical plane passing through the axis. Top row: experiments at  $Re = 3 \times 10^5$ ; bottom row: numerical simulations at  $Re = 10^5$ ; same colorbars. Left column:  $u_x$ ; central column:  $u_y$ ; right column:  $u_z$ . Horizontal axis:  $x$ ; vertical axis:  $z$ .

data. We perform 15 rotation periods at  $Re = 5 \times 10^4$  in the ANTI configuration, but we reduce the angular velocity of the top impeller by setting  $f_1 = -\frac{1}{2}f_2$  with the Reynolds number defined with respect to the angular velocity of the bottom impeller only. Then we do 10 more rotation periods with  $f_1 = 0$ ,  $f_2$  being un-

changed. After 10 rotation periods, the structure of the mean flow shifts from two recirculation cells to a single recirculation cell. The angular velocity of the top impeller is then increased so as to match the angular velocity of the bottom impeller: 5 rotation periods are done with  $f_1 = -f_2$ . Finally the Reynolds number is



**Fig. 11.** Time and azimuthal averaged velocity field in the symmetric ANTI configuration. Experiments at  $Re = 3 \times 10^5$ ; numerical simulation at  $Re = 10^5$ : (a)-(d) radial component  $u_r$ , (b)-(e) azimuthal component  $u_{\theta}$ , (c)-(f) vertical component  $u_z$ .



**Fig. 12.** Radial profiles of  $u_\theta$  and  $u_z$  for the time-averaged experimental and LES velocity fields ( $m = 0$ ) in the symmetric ANTI configuration at  $Re = 3 \times 10^5$  for the experiment and  $Re = 10^5$  for the computation:  $\langle u^{\text{exp}} \rangle_\circ$  in solid line with errorbars,  $\langle u^{m=0} \rangle$  in dashed line. Color labels are defined in Fig. 6.

increased to  $Re = 10^5$  and 12 periods are done at this Reynolds number.

We show in Fig. 13 the averaged velocity fields in a meridian section at  $Re = 10^5$  for the LES computations and at  $Re = 3 \times 10^5$  for the experiments. We clearly see that the mean flow is composed of one large recirculation cell only, which is very different from the symmetric case. Here again, the numerical results agree reasonably well with the experimental observation despite the SPIV's being blind to the impellers and to the boundary layer at  $r = 1$ .

This statement is supported by inspecting the radial profiles shown on Fig. 14. The profiles of the azimuthal component of the velocity from the numerical and from the experimental data do not coincide precisely but they have similar shapes; we observe in particular that  $u_\theta$  is mostly negative at the three vertical heights  $z \in \{-0.4, 0, 0.4\}$ . The agreement on the vertical component of the velocity is significantly better; the vertical profiles are almost invariant with respect to  $z$ . The behavior of  $u_\theta$  and  $u_z$  indicates that only one cell is present and that it is the bottom impeller that imposes its sense of rotation.

### 5.3. Torque vs. $Re$

We now compare the measurements and the numerical computations of the non-dimensional torque  $K_p$  defined in (18). (Recall that  $K_p$  also measures the dissipation power as discussed in Section 4.1.2.) All the results are reported in one single graph shown in Fig. 15. We show there the experimental measurements and the numerical estimations of  $K_p$  as a function of the Reynolds numbers over the range  $Re \in [10, 10^6]$ . The grey symbols, crosses and stars correspond to measurements. The circles correspond to numerical simulations; empty circles are for DNS simulations and yellow-filled circles are for LES simulations. We observe three plateaus at large Reynolds numbers. The blue line (bottom horizontal line) corresponds to data from the CONTRA configuration, the red line (middle horizontal line) corresponds to data from the symmetric flow in the ANTI configuration, and the green line (top horizontal line) corresponds to data from the bifurcated flow in the ANTI configuration.

For  $Re \leq 4 \times 10^2$  the CONTRA configuration (blue symbols) and the ANTI configuration (red symbols) give the same torque, both in the numerical simulations and in the experiments. The two curves split at  $Re \sim 4 \times 10^2$ . The torque for the CONTRA configuration seems to decrease monotonously with respect to the Reynolds number over the entire range of Reynolds numbers and to converge to an asymptotic value  $K_{\text{CONT}}^\infty \sim 0.05$  at very large values of

$Re$ . After reaching a minimum in the range  $Re \in [5 \times 10^2, 5 \times 10^3]$ , the torque for the ANTI configuration grows again after  $Re = 10^3$  and seems to converge towards an asymptotic value  $K_{\text{ANTI}}^{2,\infty} \sim 0.14$  at very large values of the Reynolds number. These asymptotic values of the torque coincide with experimental measurements in liquid sodium ( $Re \sim 10^7$ ) and in superfluid Helium, see [36] and [40].

The bifurcation in the ANTI configuration discussed in Section 5.2.2 and Section 5.2.3 occurs around  $Re \approx 10^4$ . The bifurcated ANTI solution is composed of one recirculation cell rotating somewhat in phase with one of the impellers [7,38]. The bifurcated ANTI flow dissipates far more energy than its symmetric counterpart. The probable cause for this higher energy dissipation rate is that the velocity undergoes very large shears in the vicinity of the top impeller as can be seen in Fig. 13(e). Actually this simulation requires a finer meridian grid and a larger number of azimuthal modes than the symmetric ANTI flow. The mesh refinement in the meridian section is done locally in the vicinity of the top impeller (see Table 4). The torque applied to the bifurcated ANTI flow seems to converge to the asymptotic value  $K_{\text{ANTI}}^{1,\infty} \sim 0.56$  for large values of  $Re$ .

Overall the experimental measurements and the numerical estimations coincide up to 10 percents over the entire range of Reynolds numbers explored and for the two forcing conditions, including in the bifurcated case. The fact that we have been able to reproduce the bifurcated branch and to estimate accurately the torque (i.e., the dissipation power) at  $Re = 10^5$  is quite remarkable considering that we are using a LES model in this range. This means that the LES model dissipates the energy properly. The method stabilizes the computation without introducing excessive numerical dissipation; i.e., the energy is allowed to cascade freely and is dissipated at the smallest mesh scale at the correct rate. To the best of our knowledge, it is the first time that numerical simulations reproduce such bifurcated branches of turbulent flows.

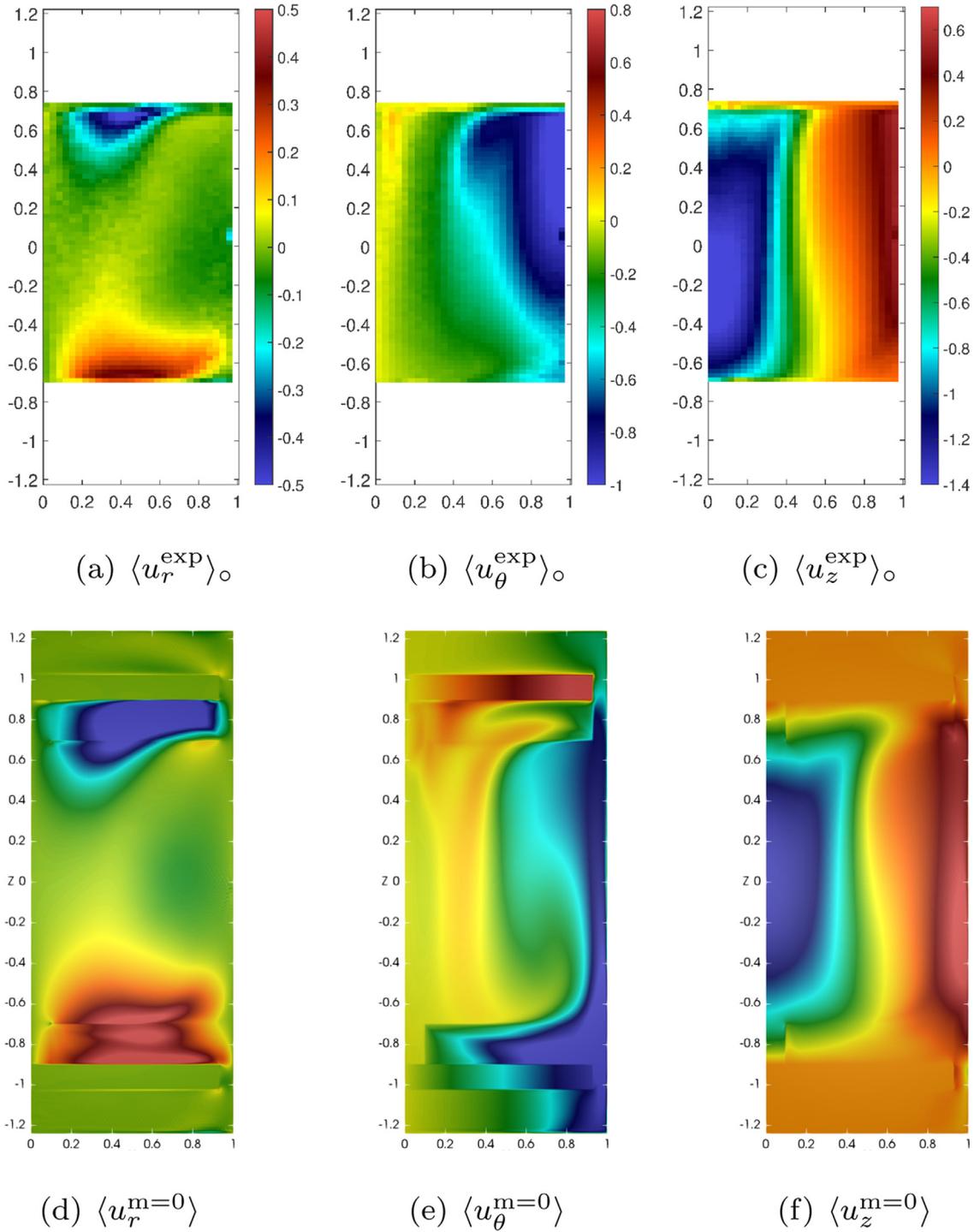
## 6. Energy spectra

This section investigates the energy spectra of the numerical simulations done at  $Re = 10^5$  using the LES model. The results are interpreted in the context of the previous studies [8,40].

### 6.1. Spatial spectrum

In 3D periodic numerical simulations it is common to compute the spatial energy spectrum as:

$$E(\mathbf{k}) = \left\langle \int \mathbf{u}(\mathbf{x}, t) \cdot \mathbf{u}(\mathbf{x} + \mathbf{r}, t) e^{i\mathbf{k} \cdot \mathbf{r}} d\mathbf{r} \right\rangle_{\mathbf{x}, t}. \quad (22)$$



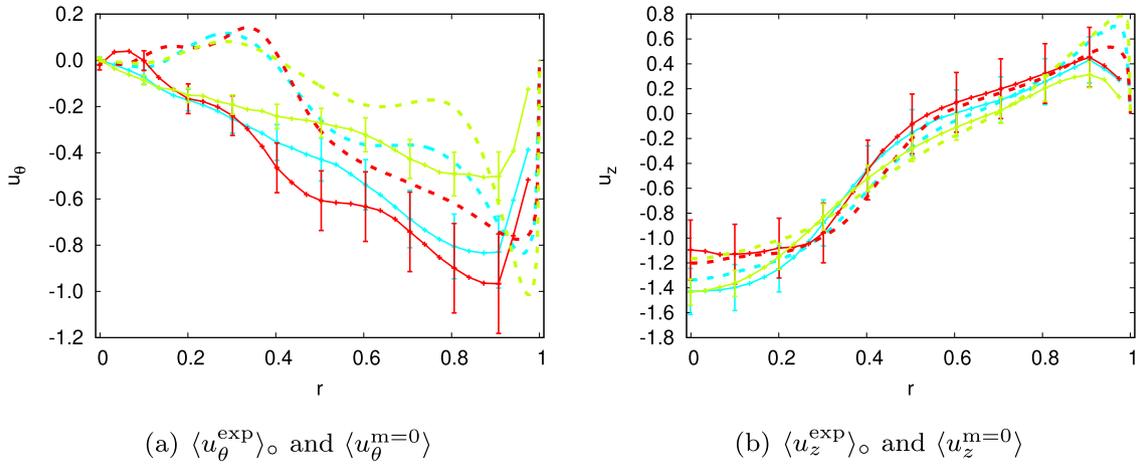
**Fig. 13.** Time and azimuthal averaged velocity field in the bifurcated ANTI configuration. Experiments at  $Re = 3 \times 10^5$ ; numerical simulations at  $Re = 10^5$ : (a)-(d) radial component  $u_r$ , (b)-(e) azimuthal component  $u_{\theta}$ , (c)-(f) vertical component  $u_z$ .

Since for isotropic flows  $E(\mathbf{k})$  only depends on  $\|\mathbf{k}\|$ , it is therefore natural to consider:

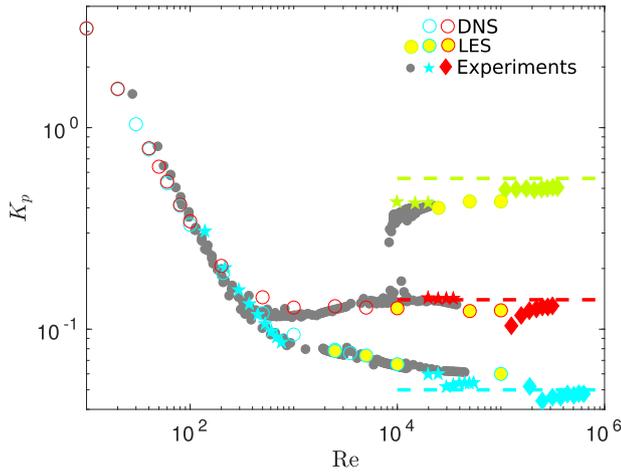
$$E(k) := \langle E(\mathbf{k}) \rangle_{\|\mathbf{k}\|=k}. \tag{23}$$

We use the LES simulations at  $Re = 10^5$  to estimate  $E(k)$ . The value of  $E(k)$  is computed from snapshots of the numerical velocity field extracted from the cube  $(-\frac{1}{2}, \frac{1}{2})^3$  located at the center of the tank. The spectra are averaged over the snapshots. The energy spectrum  $E(k)$  is supposed to scale as  $k^{-5/3}$  in homogeneous isotropic turbulence. For the family of von Kármán flows considered in the paper,

[40] suggests the universal scaling function  $E(k)/(\epsilon^{2/3} \eta^{5/3}) = f(k\eta)$  where  $\epsilon = \frac{2R}{\pi H} K_p$  and  $\eta = (Re^3 \epsilon)^{-1/4}$ . Fig. 16 shows  $E(k)/(\epsilon^{2/3} \eta^{5/3})$  for the three flow configurations. The low wavenumbers correspond to large scales and the large wavenumbers correspond to the inertial range. We observe that in the inertial range the spectra are in agreement with the  $k^{-5/3}$  law (see dotted line on Fig. 16). Note that the ANTI bifurcated flow has much less energy than the CONTRA and symmetric ANTI flows in the low wavenumber region. Recall that the ANTI bifurcated flow is essentially composed of one recirculation cell with a thin region where the velocity gradients



**Fig. 14.** Radial profiles of  $u_\theta$  and  $u_z$  for the time-averaged experimental and LES velocity fields ( $m = 0$ ) in the bifurcated ANTI configuration at  $Re = 3 \times 10^5$  for the experiment and  $Re = 10^5$  for the computation:  $\langle u^{\text{exp}} \rangle_\circ$  in solid line with errorbars,  $\langle u^{m=0} \rangle$  in dashed line. Color labels are defined in Fig. 6.



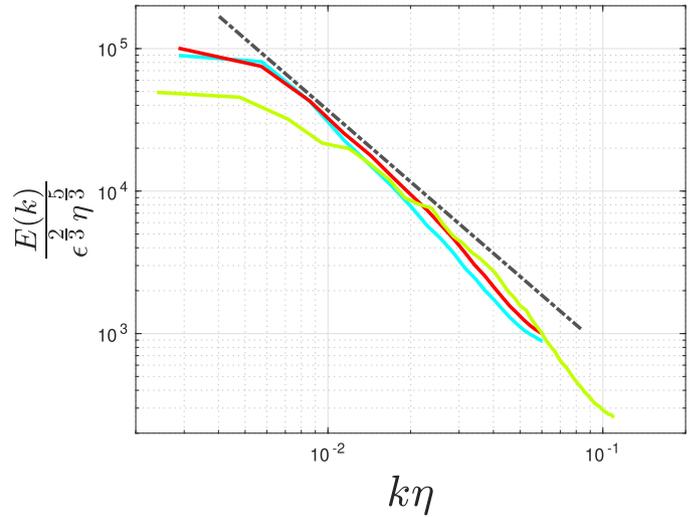
**Fig. 15.** Non-dimensional torque  $K_p$  as a function of  $Re$  for different forcing conditions: blue is for the symmetric CONTRA branch, red for the symmetric ANTI branch, and green for the bifurcated ANTI branch. Circles are numerical simulations with TM87 (empty circles are for DNS and yellow-filled circles are for LES). The other symbols correspond to other experimental results: stars are TM87 experiments using a mix of glycerol and water and diamonds are TM87 experiments with water. Grey dots are TM60 experiments (same impellers but with 16 blades rather than 8) with a mix of glycerol and water from [38]. Dashed lines correspond to asymptotic values measured in liquid sodium ( $Re \sim 10^7$ ) and in superfluid Helium 4 at 2.3 K obtained from the SHREK experiment. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

are very large, see the region  $0.6 \leq z \leq 0.8$  in Fig. 13. The slopes of the lines fitting best these curves in the inertial zone are  $-1.7$  for the CONTRA case (for  $3 \cdot 10^{-3} \leq k\eta \leq 4 \cdot 10^{-2}$ ),  $-1.6$  for the symmetric ANTI (for  $3 \cdot 10^{-3} \leq k\eta \leq 4 \cdot 10^{-2}$ ), and  $-1.7$  for the bifurcated ANTI case (for  $2 \cdot 10^{-3} \leq k\eta \leq 1 \cdot 10^{-1}$ ).

### 6.2. Temporal spectra

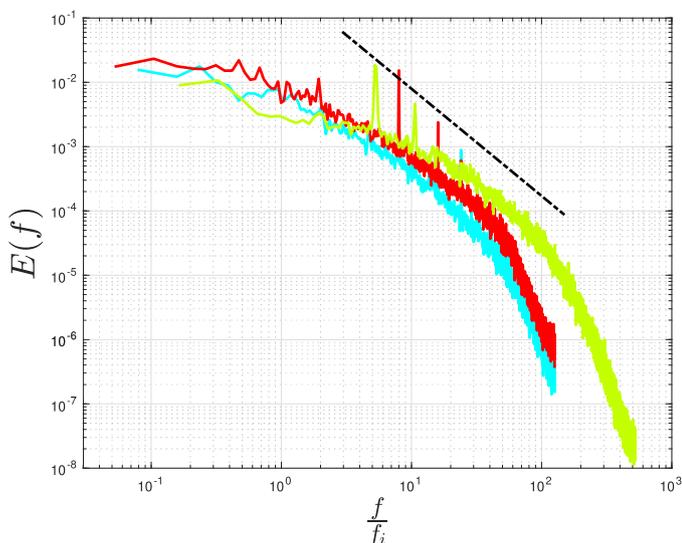
In addition to spatial spectra, one can also compute temporal spectra from time series of velocity measurements at a fixed point. Following [8] we select the following point  $\mathbf{x}_0$  ( $r = 0.9$ ,  $\theta = 0$ ,  $z = 0$ ) in the computational domain. The power spectral density (PSD) is then defined as:

$$E(f) = \left\langle \int u_\theta(\mathbf{x}_0, t) u_\theta(\mathbf{x}_0, t + s) e^{-2i\pi f s} ds \right\rangle. \quad (24)$$



**Fig. 16.** Energy spectrum  $E(k)$  as a function of the wavenumber  $k$  for different forcing conditions at  $Re = 10^5$ : blue is for the symmetric CONTRA branch, red for the symmetric ANTI branch, and green for the bifurcated ANTI branch. Dotted line corresponds to  $k^{-5/3}$ . (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

For the ANTI configuration and  $Re \leq 6.5 \times 10^3$ , [8] observed the power-law  $f^{-1}$  in the low-frequency regime (below the impeller frequency  $f_i$ ) and the power-law  $f^{-5/3}$  in the inertial range (above the impeller frequency  $f_i$ ). Note that the power-law  $f^{-1}$  is difficult to observe because it requires very long statistics. Fig. 17 presents the PSD extracted from the numerical simulations at  $Re = 10^5$  for the three flow configurations. Depending on the configuration, the time integration window in (24) ranges from 10 to 20 rotation periods. We observe in Fig. 17 three regions in the frequency domain: (i) There is a low frequency range corresponding to slow motions of the shear-layer in the CONTRA and symmetric ANTI cases; (ii) There is the intermediate inertial range. In this range the spectra behave like  $f^{-5/3}$ ; (iii) There is the large frequency range corresponding to the dissipation zone. Slope fitting in the inertial range gives  $-1.7$  for  $1 \leq f/f_i \leq 50$  in the CONTRA case,  $-1.5$  for  $1 \leq f/f_i \leq 50$  in the symmetric ANTI case, and  $-1.7$  for  $6.5 \leq f/f_i \leq 125$  in the bifurcated ANTI case. These slopes are in agreement with the Kolmogorov exponent.



**Fig. 17.** Power spectral density  $E(f)$  of  $u_\theta(\mathbf{x}_0, t)$  for different forcing conditions at  $Re = 10^5$ : blue is for the symmetric CONTRA branch, red for the symmetric ANTI branch, and green for the bifurcated ANTI branch.  $f$  is the analysis frequency and  $f_i$  is the impeller rotation frequency. The dashed line shows the behavior  $f^{-5/3}$  in the inertial range. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

## 7. Conclusion

In this paper, we have compared experimental data and numerical simulations (DNS & LES) for a complex turbulent system which is sometimes humorously referred to in the literature as the “French washing machine.” We have successfully reproduced numerically the different flow types observed experimentally in the CONTRA configuration and in the ANTI configuration. We have been able to reproduce the bifurcation observed at high Reynolds numbers in the ANTI regime: there is a turbulent symmetric solution whose temporal average consists of two recirculating zones that are invariant under the  $\mathcal{R}_\pi$  transformation, and there is a bifurcated solution whose temporal average consists of one recirculation cell only. We have focused our comparisons on two criteria: the torque value and the flow topology at various Reynolds numbers. The qualitative comparisons of the flows show good agreements between the numerical simulations and the experiments, except near the edges of the experimental measurement area. The measurements and the numerical computations of the torque coincide over a wide range of Reynolds numbers for the three flow types. Obtaining similar outputs for criteria that are so dependent on forcing conditions makes the comparison a successful one. Moreover spatial and temporal spectra computed at  $Re = 10^5$  for the three configuration flows show an inertial range compatible with the  $-5/3$  Kolmogorov exponent characterizing fully turbulent flows.

This study also proves the effectiveness of the proposed entropy viscosity stabilization as a LES model. The simulations reported in the paper validate the performance of the proposed model on a highly anisotropic turbulent flow in a complex geometry that is time-dependent with counter rotating motions that make the geometry complex in any referential. The entropy viscosity model involves two parameters  $c_{\max}$  and  $c_e$  (see Section 3.4), but we have observed that the following choice  $(c_{\max}, c_e) = (1/8, 1)$  is robust in the sense that it performs well independently of the problem. In contrast to other LES models, like the model of [41] which involves a parameter that needs to be tuned depending of the problem ([42,43]), the robustness of the entropy viscosity stabilization

with respect to  $(c_{\max}, c_e)$  facilitates its use on a wide range of problems.

## Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

## CRediT authorship contribution statement

**L. Cappanera:** Methodology, Software, Writing - original draft, Writing - review & editing. **P. Debue:** Investigation, Writing - original draft, Writing - review & editing. **H. Faller:** Methodology, Software, Writing - original draft, Writing - review & editing. **D. Kuzzay:** Investigation, Writing - original draft, Writing - review & editing. **E-W. Saw:** Investigation, Writing - original draft, Writing - review & editing. **C. Nore:** Methodology, Software, Writing - original draft, Writing - review & editing. **J.-L. Guermond:** Methodology, Software, Writing - original draft, Writing - review & editing. **F. Daviaud:** Investigation, Writing - original draft, Writing - review & editing. **C. Wiertel-Gasquet:** Investigation, Writing - original draft, Writing - review & editing. **B. Dubrulle:** Investigation, Writing - original draft, Writing - review & editing.

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